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June 1964

TECHNICAL PUBLICATION

PHOTOGRAPHIC EVALUATION REPORT
MISSION 1004-2
19-22 FEBRUARY 1964

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SYNOPSIS

Mission 1004-2 (system J-5) was the second payload recovered from vehicle No 1174. The first photography exposed on this mission was on pass D49 after ejection of the "A Bucket" (Mission 1004-1). Mission 1004-2 accomplished 64 revolutions of which 32 were operational (photography was accomplished). The payload consisted of 5,858 panoramic frames (2,909 FWD, 2,949 AFT). Seventy-five feet of stellar index film and 135 of film exposed in the terrain index camera was recovered. The characteristics of the photographic take in regard to the panoramic cameras is very similar to that of Mission 1004-1, which is considered to be a good mission.

The panoramic cameras used on this mission operated well with the exception of softspots on the master take and a few other minor degradations.

Due to the large difference in densities recorded within a pass, portions of 19 passes of the master and 25 passes of the slave panoramic camera positives were reprinted at a special density for the PI's.

The weather was exceptionally good during this mission, with only 32.5% cloud cover. Another factor that lends to the favorable overall average of the mission is that exposures were generally made while the solar elevation was favorable.

The stellar index camera operated poorly throughout the mission. When functioning correctly, stars to the fifth magnitude could be discerned.

The terrain index camera functioned well.

The horizon cameras generally operated well but the port horizon appeared to be consistently underexposed.

GENERAL FLIGHT DATA

Date of Launch: 15 February 1964 Orbital Parameters:

	1 41	111166
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Actual (Revolution 92)

Period: 90.07 min Perigee: 100.0 nm Perigee tatitude: (Not Available) Apogee: 236.0 nm Eccentricity: 6.019 Inclination Angle: 75° 90.78 min 102.38 nm 43.25° north :245.51 nm 0.0198 75.06°

PART I. CAMERA OPERATION

1. Master (FWD) Panoramic Camera No 124: This is the same camera used in Mission 1004-1. Therefore, as would be expected, the characteristics of the photographic take are very similar. The photography is highly degraded, due to image softness, in an area approximately 1.0" wide along the camera number edge in the first 3 to 15 frames of nearly every pass. This soft

imagery extends from 3.0" to 8.0" from the take-up end of the affected frames. There are three small emulsion digs just inside the format adjacent to the camera number on every frame. A minor emulsion abrasion extends edge to edge in line with each dig.

Minor corona static discharges and occasional minor associated equipment shadow-

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graphs appear intermittently near the center of the format.

A group of short, fine emulsion scratches parallel to the major axis of the film begins approximately 1.5" from the take-up end of each frame and extends approximately 3.0" toward the supply end. Thin, random, longitudinal emulsion scratches are frequent throughout the mission. Rail scratches are severe from head to tail.

A diagonal streak of fog extends into the format from the untitled edge on the third frame of most passes. The existence and density of the fog is dependent on the duration of the camera-off period.

The camera speed had a tendency to be slow on the first frame of some passes near the end of the mission, resulting in image smear as well as gross overexposure.

2. <u>Slave (AFT) Panoramic Camera No 125:</u> This camera was operational throughout the mission and, like the master camera, is the same unit used in Mission 1004-1.

Frames 29 thru 38, pass D49 of Mission 1004-1, which were recovered in this payload capsule, were severely damaged at the processing site.

Random longitudinal emulsion scratches are intermittent throughout the mission. Rail scratches are continuous from head to tail.

There is corona fog at the take-up end of the third or fourth frame of nearly every pass. The resulting degradation is minor.

A light leak resulting in a diagonal streak of fog emitted from the titled edge affects the fifth frame of nearly every pass. The existence and density of this fog is associated with the duration of the camera-off period.

Beginning at pass D86 there are from 1 to 3 random minus density spots approximately 0.1" in diameter on nearly all subsequent frames. Some of these spots are apparently the regult of

a roller-induced film crimp. The reason for others has not been determined.

3. Master (FWD) Horizon Cameras:

a. The port (supply)horizon camera operated normally through pass A71E. Horizon images, fiducials, binary words and end-of-pass markers do not appear on passes D72, frame 54; D85, frame 75; D87, frame 136; D103, frames 57 and 133. Underexposure prevails at the beginning of most passes but improves on passes which occur over areas of high solar elevations. All horizon images are slightly vignetted in two corners. Where the exposure is sufficient to permit analysis, acuity is very good.

b. The starboard (take-up) horizon camera operated normally through pass A71E. Horizon images, fiducials, the binary words and endof-pass markers do not appear on pass D72, frame 54; D85, frame 75; D87, frame 136; D103, frames 57 and 133. When operational, the exposure was adequate and the acuity is very good. As in the port cameras all horizon images are slightly vignetted. There is a small plus density area at the edge of the format opposite the horizon image which is believed to be a reflection.

4. Slave (AFT) Horizon Camera:

a. The starboard (supply) horizon camera functioned normally throughout the mission. Some imagery is slightly vignetted on every format. The exposure was adequate and the acuity is very good.

b. The port (take-up) horizon camera functioned normally throughout the mission. The first few frames of most passes were underexposed but as the solar elevation improved the exposure became adequate.

The two west-looking (starboard) horizon cameras were set at f/8.0, 1/100 second with Wratten 25 filters and the east-looking (port) cameras were set at f/6.8, 1/100 second and equipped with Wratten 25 filters. The east horizon, photographed with the port camera, was

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often underexposed due to the unfavorable solar elevations. Horizon imagery in all four cameras is slightly vignetted but the vignetting does not hinder the useability of the horizon arcs for vehicle attitude determination. The design of the horizon cameras now employed is such that slight imagery vignetting will always be present.

- 5. Stellar Index Camera No D42/42/37: The camera operated erratically throughout the mission. There were eight double exposures during the course of the mission and 57 frames were grossly overexposed and unusable due to the shutter hanging open. The shutter also remained open while the film was being advanced on 53 occasions. Due to the shutter not opening or not opening long enough to form an image, 25 frames are clear in the first 350 programmed. There were no stellar images after frame 350. The program called for 407 frames. The correlation fiducial lamps did not function during the mission. Edge static is continuous on both edges throughout. A diagonal plus density band, attributed to a light leak, is apparent on nearly every frame. The moon is imaged on frames 298-355.
- 6. Terrain Index Camera No D42/42/37: The camera operated normally throughout the mission with the exception of a double exposure on frame 5. The imagery recorded is of good quality except for 8 frames affected by a minor light leak.

7. Collateral Equipment:

a. The 200 cycles per second (cps) frequency marks are present on all frames throughout the mission. On the Master (FWD) cameras, the marks are imaged in the format and, being superimposed on the terrain imagery, are not

readable except on engineering passes and passes where the imagery is of low density. The frequency marks are printed outside of the terrain format on the slave panoramic camera but are reflected into the format edge. However, they are readable throughout and the reflection does not seriously degrade the pan camera imagery.

- b. Light number 11 of the binary data block on the slave camera did not function during the mission. Light number 14 failed on frame 92 of pass D85 and on all subsequent frames. The binary data block of the slave camera tracks into the panoramic format on most frames. The binary data block of the master camera was operational and readable throughout except on pass D72, frame 54; D85, frame 75; D87, frame 136; D103, frames 57 and 103. The images of the data block on both cameras is slightly bloomed.
- c. The terrain and stellar index camera correlation fiducial marks failed to operate during the entire mission.
- d. The camera-off marker of the slave camera recorded satisfactorily through pass D56. On passes A56E, A71E and A72E it is superimposed on the binary word. The camera-off marker of the master camera recorded satisfactorily throughout pass D55. The mark is superimposed on the binary word in passes A55E, A56E and A71E. On all passes after A71E, the end-of-pass marker is misplaced and usually appears over the first frame of the following pass.
- e. The camera numbers, although bloomed, are recorded and readable throughout.

PART II. FILM

1. <u>Film Processing</u>: This section provides a descriptive evaluation of the exposure and the

processing, and comments on the exposure, the density, the processing and the physical condi-

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tion of the original negative.

Pertinent data was collected during various phases of the processing and more thoroughly during the evaluation of the negatives. This is a standard procedure. The community is informed by cable of any extensive defects in the photography which may affect the PI suitability of any mission.

Support organizations provided the processing center with pre-launch samples of the actual film used on this mission. These samples, along with fresh process control stock, were sensitometrically exposed and processed at controlled levels of development. A characteristic curve was prepared from these sensitometric strips and is defined as the "Mission Material Processing Curve."

While the film was being prepared for processing, it was inspected for physical damage which could cause processing difficulties. During processing, data was recorded giving the processing conditions and film footage locations where processing changes occur. Changes in the normal course of processing which may affect the film quality were recorded and, after processing, the original negatives were examined frame by frame for defects and damage.

Most of the film on this mission received adequate exposure. The solar elevation varied from a low of -55° on engineering passes A103E and A104E and -5° on operational pass D66 to a high of 68° on pass D103. Acceptable photography was accomplished with a minimum solar elevation of approximately 4°47' in pass D67, at a latitude of 71°30' north. The local time at which the exposure was made was 0942. The photographs taken at the lower latitudes, where the sun was relatively high (30°-40°), tend to be slightly overexposed. The greatest variation of density that is directly attributed to exposure is in the horizon images. On the majority of frames from both FWD and AFT panoramic cameras the

port horizons did not have optimum exposure. The starboard horizons were properly exposed rendering adequate density throughout most of the mission.

The exposure of the stellar index camera appears to be near optimum where not degraded by the various shutter problems. The exposure of the terrain index camera also appears to have been near optimum.

Approximately 50% of the film exposed in the pan cameras received intermediate development, 13% full, and 37% primary. Because of exposure changes duesto variations in sun elevation and terrain, approximately 50 changes in the development level were made during the processing of the slave film and approximately 65 changes during the processing of the master film. The gross fog density readings range from a minimum of 0.07 to a maximum of 0.21.

The film from both the stellar and terrain index cameras was processed normally.

The density of the pan camera photography is near optimum considering the latitude of terrain reflectivities encountered on the mission.

2. Film Degradations: This section lists some of the more notable film degradations and a few frames on which examples of each can be found.

a. Master (FWD) Panoramic Camera:

Corona

Small corona discharges are evident in the horizon format of several frames after pass D49. (Examples: pass D50, frames 1, 2, 20.) Minor corona bursts are also common on the third frame after a camera-on position. Examples of this may be found on pass D52; A71E, and D78. On pass D64 and on all subsequent passes corona discharges become more frequent and appear at intervals of approximately 6.3%. (Example: D64, frame 35 Fwd.)

Light Leaks

A diagonal band of plus density resulting from a light leak appears on the fourth frame of each pass. The

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film suspended in the camera during a camera-off position often is slightly fogged, depending on the duration of the camera-off period and the solar elevation during the period. (Example: pass D94, frame 1.)

Manufacturing Splices tain fogging and equipment images due to light leaks within the system. (Example: pass A104E.)

Emulsion Digs .

Four small emulsion digs are present adjacent to the camera number just inside the format at each edge.

σ ; Minus Density Pass D55, frame 35; pass D71, frame 110.

Minus Density Streaks Faint minus density streaks appear on frames 2-22 of pass D67.

Comets

Appear at random throughout the mission. (Example: D71, frame 36.)

Dendritic Static

Small, minor discharges are present occasionally in the third frame following a camera-on position. (Example: A72E, frame 3.)

Emulsion Scratches Rail scratches are continuous and severe. Longitudinal emulsion scratches appear intermittently throughout the mission, and on pass

Manufacturing Splices Pass D49, frame 15; pass D68, frame 167; pass D102, frame 87.

Creases and

throughout the mission, and on pass D49, Mission 1004-1.

Minus Density Comets Excessive and pronounced throughout the mission. (Examples: D71, frame 36.)

Tears

Severe creasing, tearing, etc., occurred on Pass D49, Mission 1004-1 at the processing site to such an extent that small pieces of film were completely destroyed. A series of crimps and creases appear on pass D103, frames 96-95. Severe film damage occurred on the last 3 frames of pass D112 as the loose end of film was drawn through the camera.

Emulsion Scratches Rail scratches are severe and continuous. Several short, longitudinal emulsion scratches appear within a 3.0" band edge to edge beginning approximately 3.0" from the take-up end of each frame. (Example: De2, frame 15.) Pass D111, frames 26-25 were severely scratched as loose film was drawn through the camera.

Blisters

Some of the aforementioned minus density comets were definitely the result of blisters. They are moderate in number but serious in nature.

Blisters and Pinholes Minor and Intermittent.

Image Smearing

This is common on the first 6 frames of most passes on frames exposed before the system overcame inertia. (Example: D62, frames 1-6.)

Pinholes

Minor and intermittent except on pass D71 where they are numerous and associated, with the manufacturing splice on frame 110.

b. Slave (AFT) Panoramic Camera:

Corona Static

There is usually a small discharge on the third frame after a camera-on position. (Example: D64, frame 3.) Pass D66 contains random discharges throughout. Minus Density Špots A minus density spot approximately 0.15" in diameter appears intermitently 0.8" from the frequency mark edge on pass DS6, frame 7 and on most subsequent frames. Another minus density pattern, in the shape of a half-moon with a tail projected from its concave surface, also begins on pass DS6, frame 7 and appears intermittently throughout the remainder of the mission. The spot is approximately 0.1" by 0.1" at the extremes

and a small plus density is often noted in the center of the half-moon area. The pattern is suggestive of a crimp.

Light Leaks

There is a plus density hand caused by a light leak on the fourth frame after each camera on position. Several patterns of fog are present on pass D49 (Mission 1004-1). This apparently is associated with the cut and wrap operation. The first and last few frames of most passes con-

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c. Stellar Index Camera:

Edge Static Corona and dendritic static discharges along both edges are continuous.

There are random static discharges

within the format.

Light Leak A diagonal band of fog appears on nearly every frame and is very dis-

tinct on 22 frames.

d. Terrain Index Camera:

Edge Static

Static discharges are continuous along

both edges.

Corona

Frame 16 only.

Light Leaks

A band of fog projects into the format from the camera number edge of frames 19, 21, 29, 45, 49, 67, 74 and 81.

PART III. IMAGE QUALITY

1. Photographic Interpretation (PI) Suitability: This is an assessment of the information content of photographic reconnaissance material and its interpretability. A number of interrelated factors are involved, such as the quality of the photography, the extent of target coverage, scale, weather limitations, and similar considerations. However, the fundamental criteria for assigning a PI suitability rating may be reduced to (a) the scope of the photographic coverage and (b) the degree to which a photo interpreter may extract useful and reliable information from the material.

PI suitability ratings are categorized as Excellent, Good, Fair, Poor, and Unusable. These ratings refer to the overall interpretive value of the photography obtained from a particular reconnaissance mission. Individual targets may also be assigned PI suitability ratings if that is necessary or desirable. The standards that determine assignment of the various ratings are as follows:

Excellent: The photography is free of degradation by camera malfunctions or processing faults and weather conditions are favorable throughout. The imagery contains sharp, well-defined edges and corners with no unusual distortions. Contrast is optimal and shadow details, as well as details in the highlight areas, are readily detectable. Observation of small

objects and a high order of mensuration are made possible by the consistently good quality of the photography.

Good: The photography is relatively free of degradation or limiting atmospheric conditions. Edges and corners are well-defined. No unusual distortions are present. Detection and accurate mensuration of small objects are feasible, but to a lesser degree than in material rated as "Excellent".

<u>Fair</u>: Degradation is minimal but the acuity of the photography is less than optimum. Edges and corners are not crisply defined and there is loss of detail in shadow and/or highlight areas. Detection and identification of small objects are possible but accuracy of mensuration is reduced by the fall-off in image quality and the less-than-optimal contrast that prevails.

<u>Poor</u>: Camera-induced degradations and/or weather limitations severely reduce the effectiveness of the photography. Definition of edges and corners is not sharp. Only gross terrain features and culture may be detected or identified and distortion of form may exist. Accurate mensuration of even large objects is doubtful.

<u>Unusable</u>: Degradation of photography completely precludes detection, identification and mensuration of cultural details.

2. PI Suitability for Mission 1004-2: The PI

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suitability for this mission is considered to be good in that fine detail is readily discernible through most of the mission. Photo interpreters reported on 140 targets in the preliminary target read-out of which 9% were given quality ratings of poor and the remainder a rating of good. Snow was the degrading factor on 6% of the targets receiving poor ratings while haze was to blame for the remaining 3%. Highlights of the mission coverage are as follows:

- a. Discovery of construction and activity observed at a missile test center.
- b. Discovery of construction at a nuclear weapons proving ground.
- c. Clear count of aircraft at a military airfield.
 - d. Identification of a radar array.
- e. Discovery of a large area of new construction.

Mission 1004-2 produced imagery only slightly inferior to the best ever attained by the KH-4 system. The degradations that are present and the problems encountered that have a direct bearing on PI suitability are as follows:

<u>Corona Static</u> - The degradation of imagery due to the effects of corona discharge is minor on both panoramic cameras.

Light Leaks - Diagonal patterns and equipment shadowgraphs are usually present on one or more of the first five frames and on the last three frames of each pass on both the master and slave panoramic cameras. The fog caused by the light leaks is minor but it does have a degrading effect. A good example of the various fog patterns may be observed on pass D64, frames 4 and 5. These light leaks are a result of the camera design and are not an anomaly.

Scratches and Abrasions - Four small emulsion digs at each edge of the format, adjacent to the camera number, appear on most frames of the master camera. Although these digs are small, had a target fallen in this area,

it would have been degraded or lost.

Atmospherics - 32.6% of the photographic take of this mission is obscured by clouds. Eighty-two known targets were not reported due to atmospherics. Haze degraded 5 targets to such an extent as to be rated poor for photographic interpretation.

<u>Solar Elevation</u> - Most photography was accomplished while the solar elevation was favorable and little imagery was lost.

Image Motion - The first few frames after each camera-on position display this condition. The slow camera speed at the beginning of pass becomes more pronounced as the mission progresses. The PI suitability is highly degraded on the affected frames.

Minus Density Comets - While each comet is very small, the large number of them encountered on this mission makes them a degrading factor.

<u>Soft Spots</u> - The imagery within the area described as being of "soft focus" on the master camera is highly degraded and of little use to the PI.

The image distortions inherent in the KH-4 camera are common throughout the mission. Pass D62, frames 17 FWD and 22 AFT are good examples.

Plus and minus density streaks associated with areas of heavy density (clouds) are noted intermittently throughout the mission.

3. Mission Information Potential (MIP): The MIP is an arbitrary number, not limited by terminal values, which is subjectively assigned to the panoramic photography of a mission and which compares it to the other KH missions. It is meant to be a measure of the camera's maximum capability for recording information, dis-

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counting adverse atmospheric conditions, minimal solar elevations, camera malfunctions or other factors which reduce the quality of the photography. The MIP is based on the best photography found in a mission, even though the photography may be limited to a few frames. Since these frames are considered the best in the mission, they do not indicate the overall success, average quality, or general interpretability of the photography.

Criteria for selection of an MIP frame:

- a. Eliminate all portions of the mission affected by system malfunctions.
- b. Select frames which are free of clouds and atmospheric attenuation.
- c. Eliminate the first ten frames and last frame of a pass as these may be affected by incorrect scan speed.
- d. Select frames that are in a continuous strip of approximately ten cloud-free frames, as cloud shadows from distant weather fronts are cast for great distances.
- e. Determine from the horizon cameras that the panoramic photography is not affected by apparent vehicle perturbations.

- f. Select targets that are near the center of format and on frames as close as possible to perigee for scale purposes and to eliminate obliquity.
- g. Select frames having near optimum solar elevation, thus eliminating frames having either overexposure or underexposure.
- h. Select a high contrast target (preferably an airfield) and compare the target to a previous mission which has been given an MIP rating.
- 4. MIP For Mission 1004-2: Utilizing the criteria set forth in the preceding items, pass D62, frame 23 AFT was selected as the MIP frame for this mission. The mission was given an MIP rating of 85 and is comparable to Mission 1004-1 (also MIP 85).

The photographic scene covers a city and airfield which are located near the center of the format. Image quality is such that runway markings, aircraft engine nacelles (on larger aircraft), and vehicles in parking lots and on highways are discernible.

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APPENDIX A. SYSTEM SPECIFICATIONS

Panoramie Cameras		· · · · · · · · · · · · · · · · · · ·	Stellar and Terrain Index	Cameràs	• • • • • • • • • • • • • • • • • • • •
	Master (FWD)	Stave (AFT)		Stellar	Terrain
Camera No Lens Serial No Slit Width Aperture Filter Operational Focal Length Film Type Film Length Emulsion Static Bonch Test High Contrast Low Contrast Dynamic Test I. High Contrast P. High Contrast P. High Contrast P. Low Contrast	124 0642435 0.250" f 3.5 Wratten 21 609.60 mm 4404 7500" 45-73-12-3 290 L mm 160 L mm 170 L mm 131 L mm 153 L mm	125 1022435 0.250" f 3.5 Wratten 21 609.60 mm 4404 7500' 45-73-12-3 238 L mm 155 L mm 178 L mm 115 L mm 215 L mm	Camera No Lens Serial No Reseau Serial No Filter Aporture Exposure Time- Operational Focal Length Film Type Film Length Splices Emulsion Perpendicularity of Reseau Location of Principal Point Awar	D42-42-37 10510 37 None f 1.8 2 sec NA 4401 75' None 7-3-1-4 0.00''-0.93''	D42 '42 '37 513050 42 Wratten 21 f. '4.5 1 '500 sec NA 4400 135' None 16-4-11-3 0.00' -2.25'' NA

	Starboard	Port	Starboard	Port
	(Take-up)	(Supply)	(Supply)	(Take-up)
Panoramic Camera No	124	124	125	125
Lens Serial No	812265	812271	812276	512272
Exposure Time	1 100 sec	1,100 sec	1/100 sec	1/100 sec
Aperture	f 8.0	f.6.8	f/8.0	f 6.8
Filter Operational Focal Length	Wratten 25	Wratten 25	Wratten 25	Wratten 25
	54.45 mm	54.33 mm	58.46 mm	55.48 mm
Average Lines mm Radial Resolution (L/mm)	162 L mm	167 L. mm	111 L. mm	178 L. mm
10° off axis 20° off axis Tangential Distortion	.009 mm	015 mm	.004 mm	.002 mm
	.012 mm	015 mm	.002 mm	.009 mm
	.004 mm	Not Available	.005 mm	.003 mm

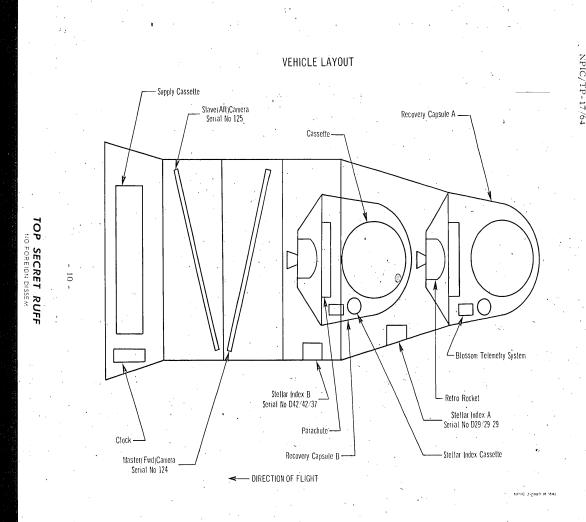
		Camera	No 124	,		
Resolution	-	Take-up	-		Supply	
Angle Off Axis Radial Resolution (L/mm) Tangential Resolution (L/mm)	0° 157 168	10° 141 141	20° 100 78	0° 157 177	10° 141 141	20° . 106 - 88

				Ç	amera	No 126			•					
Resolution	Take-up							Supply						
Angle Off Axis Radial Resolution (L/mm) Tangential Resolution (L/mm)	0° 184 164	5° 164 145	10° 144 142	15° 112 115	20° 103 56	25° 105 60	27.5° 58 44	0° 164 164	5°. 164 162	10° 162 151	15°- 134 121	20° 109 91	25° 99 60	27.5° 41 41

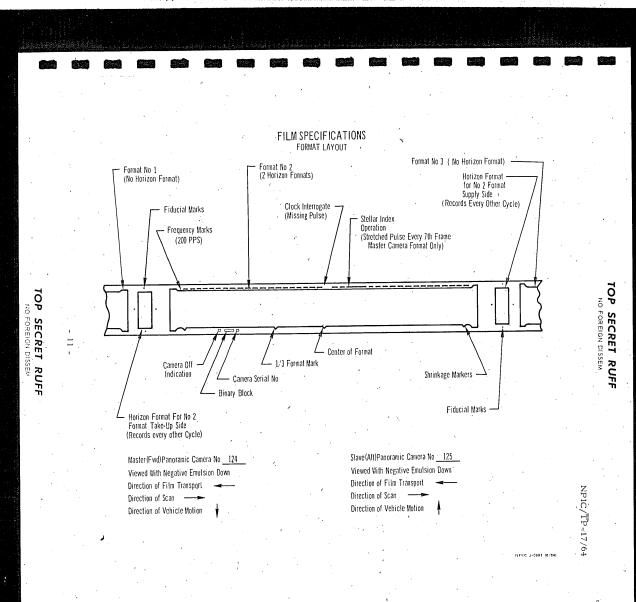
иста No D42, 42, 37			-							
Resolution			Stellar			ı		Index		-
Angle Off Axis	NA	NA	NA	NA.	NA	0°	10°	20°	30°	35°
High Contrast	NA	NA.	NA	NA	NA	73	92	105	59	77
Low Contrast	NA NA	NA	NA	NA.	NA	73	53	91	35	18

NA denotes Not Available.

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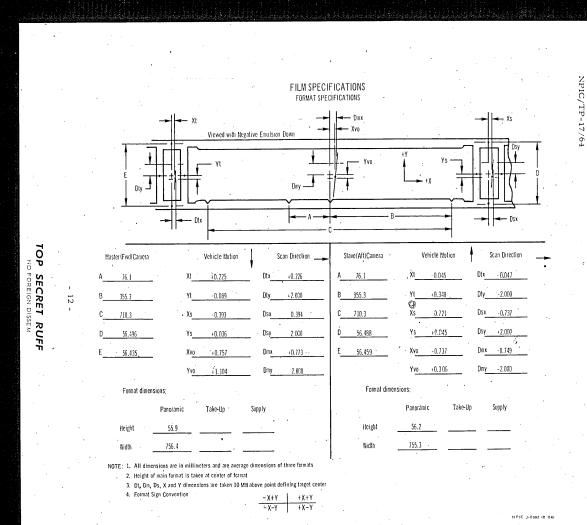


TOP SECRET RUFF





Approved For Release 2002/07/01 : CIA-RDP78T05439A000500050005-0



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TOP SECRET RUFF

NO FOREIGN DISSEM

· .. NPIC/TP-17/64

APPENDIX B. TECHNICAL COMPENDIUM

1. Master (FWD) Panoramie Camera

				·			1. Naste	T (F N D)	Panoramii	c Camera								
-												Ferrair	1		Lim	iting		
_		. "		Univ.	Sun	Solar			Yaw	- Alt.	D	D		D	D	.		1_
Puss	Frame	Over- lap	Cloud	Time	Time	Elev.	Pitch	Roll.	(All Minus)*	(yds)	Min	Max	1	Min	Max	-7	Fog	Exp
D49		N:D	20.11		4.3	51 43		NA.	- NA	NA.	NR	N. T.	7.17	0.05	.3.35	• • •		
D50	. 01	NR 06	0021 . 4212	0116	1007	-05-21	NA: 14°54	-00°07	01705	244719	0.74	NR 1.69	NR 0.95	$0.07 \\ 0.74$	$\frac{2.25}{2.05}$	1.31	0.11	NA 1. 211
D50	4.4	07	4311	0115	1116	14 36	15 02	00.12		200726	0.51	1.34	0.53	0.51	1.92	1.41	0.11	1 229
D52	58	ÙĠ	1111	0424	1220	31 51	15 10	00-25	01.42	211752	0.62	1.21	0.59	0.42	2.05	1.63	0.11	1, 256
D52	56	07	1111	0425	1229	35.39	14.05	00.35	01.25	208772	1.25	1.95	0.73	0.85		1.28	0.11	1.257
D53	06	07	1111	. 0552	1147	21.25	15.09	00.07	01.00	223759	0.59	1.95	1.06	0.57		1.19		1 208
D50	57	(10)	1111	0556	1232	36.48	15 04	00.26	NA	207148	0.95	1.99	1.01	0.95	1.99	1.01		1 257
D54	03	00	2204	0719	1027	05.26	14 47 ~	00.23	01.07	247955	0.27	0.44	0.17	0.27	2.07	1.50	0.05	1.194
D54	1.75	OG	4111	0723	1147	21.50	15/28	00.53	01.53	222733	1.07	-1.67	0.60	0.60	1.74	1.14	0.05	1 241
D54	>7	(11)	1111	0724	.1155	23 44	15 26	00.51	01.39	219022	0.83	1,51	0.65	0.66	1.65	0.99	0.05	1, 245
D54	102	NR	1111	0725	1204	25.49	15 15	00.45	NA	217022	1.35	1.59	0.24	0.60	1.71	1.11		1 247
D55	02	NR	5555	0549	1000	05.35	f4 52	-00 17	00.15	253602	NR	NR	NR	0.34	1.63	1.29	0.16	1.1156
D55	0.5	0.1	3445	0550	11005	06-02	14.55	*600 I (t	00.15	246516	NR	NR	NR	(),:):)		1.52	0.20	
D55	54	NR.	5555	0553	1136	15 20	14 25	00.10	01.02	227902	NR	NR	NR	0.75		0.52		1, 237
D55	124	06	1111	0856	1159	24 27	15 12	00 10	01 14	219145	0.75	1.55	0.50	0.75		0.55		_1, 245,
D55	160	015	1111	0856	1215	20 01	15 54	00-15	.01.09	214201	1.35	1.50	0.42	0.83	1.50	0.97		1, 253
D55	258	006	1211		.1244	42.08	14 34	00.06	00.57	205000	0.57		0.37	0.41	2.30	1.59		1 261
D56 D61	56 35.	08 NR	2111 4455°	1027	1214	29-52 NA	15 05 15 30	-00 07 -00 17	01 11 .	210492 205581	1.00	1.55 NR	0,55 NR	1.00	1.55	0.55		1 255
D62	01	- NR - 00	1111		-1310	NA 42 54-	15 25	00.05	00 55 NÅ	205551	NR 1,30	NR 1.52	0.52	0.80	2.14	0.75	0.09	1 258 NA
D02	02	00	1111	1936	1313	43 06	15 25	. 100.05	NA.	205000	0.62	1.38	0.76	0.62	1.65	1.06		1 151
Des	00	(00	1111	1906	1017	43.19	15 24	00.07	NA	204650	0.40	1.65	1.25	0.40	1.65	1.25	0.09	1. 224
D62	0.4	0.2	1111	1936	1315	43.32	15 24	00.07	NA	204500	0.45	1.42	0.94	0.45	1.72	1.24	0.11	1 240
D62	. 0.5	0.4	1111	1936	1319	43.40	15 23	00.05	NA	204500	0.65	1.58	0.90	0.65	1.82	1.14	0.11	1.246
D62	06	(0.1)	1111	1500	1319	13 40	15/20	00.05		204500	0.72	1.45	0.76	0.72	1.92		0.10	1 250
D62	17	03 .	1111	1937	1321	45 05,	15/21	00.02	00.46	204550	0.62	1.70	1.05	0.40	1.75	1.35		1. 255
Ð62	18	0.3	1111	1937	1021	45 08	15/22	00.03	00.46	204550		1.90	1.22	0.65		1.22		1255
D64	65	(0.5	1111	2225	1125	10.08	.14 34	-00.07	NA	239425	0.60	1.62	1.02	0.50	1.52	1.82	0.11	1. 224
D64	60	0.7	2222	2252	1450		- 14 40	00.20	00.56	275757	NR	NR	NR	0.45	2.21	1.73	0.11	1.192
D05	15	06	1111	2359	1049	11 32	15 26	00.12	NA NA	239035	0.61	1.55	0.97	0.60	1.54	1.24	0.11	1 229
D65 D66	49 32	- 07	1111	0001	1121	16 47 19 20 .	15 23 14 38	00.03	NA NA	[227065 225229	0.55	1.66	1.11	0.27	$\frac{1.91}{2.03}$	1.64	0.09	1. 235
D66	64	0.5	4313	0134	1445	24 11	15 37	00 03	NA . 00-31	215000	0.62		1.09	0.27 0.53	2.03	$1.76 \\ 1.61$	0.11	1. 232
D66 -	74	16	4313	0184.	1151	25 21	15 30 -	00.13	NA	247(008)	0.52		1.10			1.56	0.05	1. 245
D::7	21	10	1111	0259	0942	04.47	14.55	00.34	01.16	248400	0.65	0.90	0.22	0.46		0.56	0.20	1 214
D67	4.4	0.9	1111	0305	1200	26 01	15.08	00.23	00.45	215152	6.72	2.00	0.25	0.61	2.06	1.45		1 244
D65	45	0.0	1121	0435	1144	24.36	14.53	00.03	NA	218078	0.60	1.91	1.31	0.60	2.08	1.45	0.11	1.235
D65	6.3	10	1111	0436	1152	26.56	14 40	00 03	00.22	215889	0.55	1.65	1.10	0.55	1,94	1.06		1.1249
Del S	102	10	1112	0439	1217	36 39	14.57	00.10	01.19	207000	0.96	1.75	0.82	0.54	1.92	1.05	0.10	1 258
D⊕∽	161	05	2215	0440	1226	40,45	14 54	00.15	01 03	205500	NR	NR	NR	0.39	2.03	1.64	0.11	1-200
D-19	07	10	1111	0604	1120	1-11	15 57	00.45	NA	227049	0.54	1.66	1.12	0.54		1.42	0.11	NA
D69	4.1	69	1111	0606	1100	20, 29	15 52	00:06	NA	217449	1.04	2.00	0,96	1.04	2.16	1.12		NA
D70	ug.	09	1111	0736	1126	19.59	14 45	00.31	01-23	222921	0.76	1.52	1.06	0.76	2.02	1.26	0.21	1 235
D70	97	05	1211	0740	1215	35 54	14 34	00.25	01.02	207335	1.36		0.54	1.20	1.05	0.75		1 255
D71	0.5	67 12	1114	0.906	1121 1142	15.55	14 56	00.01	NA 00/32	224730	0.94	1.42	0.45	0.80	1.65	0.55		1 237
D72 D72	23 46	11	3121 1111	1039	1155	$\frac{24}{27} \frac{21}{55}$	15-18 15-24	-00 10 -00 05	NA	216000 216000	NR 1.00	NR 1.93	0.93	$0.26 \\ 0.72$	2.04	1.75	$0.11 \\ 0.09$	1 247 1 251.
D72	74	10	1112	1045	1205	46.39	16 04	00.05	NA.	205250	0.69		1.23	0.65	2.19	1.54	0.21	1 259
D72	- 	11	1111	1046	1241	45 15	16 01	00 19	01.05	205000	1.10	1.70	0.60	1.10	2.00		0.15	1 259
D75	05	- 10	. 1111	1947	1210	37.05	15 14	00.01	00 43	206500	NR	NR	NR	1.16	1.96			1 245
D75	25	1.1	1111	1945	1217	40.02	15 17	-00.08	NA	205500		1.44	0.26	0.52	1.00	1.35	0.09	1 258
Dan	10	0.9	1111	0315	1100	25 88	15 11	00.12	00.31	215000	0.96	1.96	1.00	0.70	1.95	1.25	0.11	1 247
D > 0	43.5	. 11	2111	0319	1151	01.02	14.50	00.19	NA	211000	1.15	1.56	0.68	1.18		0.84		1 254
D 5 3	.76	10	1211	0320	1257	26 16	14.51	100.28%	00.45	207402	0.74	1.92	1.15	0.08	2.02	1.64		1.257
D 5.5	11	1945	1111	06 I ×	1120	21.44	15 35	-700 (01	NA	218962	0.94	1.97	1.03	0,69	2.06	1.37	0.19	1 242

TOP SECRET RUFF NO FOREIGN DISSEM

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1. Master (FWD) Panoramic Camera (Continued)

	,									-	. 1	errair			Lim	iting		
Pass	Frame	Over lap	Cloud	Univ. Timé	Sun Time	Solar Elev.	Pitch	. Roll	Yaw (All Minus)*	Alt. (yds)	D Min	D Max	7	D Min	D Max	Fog	Δ	Exp
D55	51	.10	1111	0620	1141	27 47	15 26	00.24	NA ·	211596	0.42	1.74	1.32	0.41	1.55	1.47	0.11	1 251
D55	53	10	4313	. 0622	1206	37 37.	14.53	00 09	NA	2.06552	0.55	1.91	1.06	0.69	2,00	1.31	0.09	1 253
D 5 6	. 25	11	4012	0749	1121.	22 32	15 45	00.22	01.02	216000	0.55	1.57	0.99	0.86.	2.03	1.17	0.09	1. 246
D56	75.	69	1111	0752	1153	32 17		00.32	NA	209090	1.49	1.75	0.26	1.01	1.87	0.86	0.09	1 255
D56	93	09	44,12	0753	1200	34 45	15 17	00.27	00.85	207000	0.55	1.72	0.54	0.85	1.72	0.84	0.07	1 '254
D57	4.5	11	1111	0920	1128	24 00	15 04	,-00.01	NA	216976	1.15	1.96	0.78	1.15	1.95	0.80	0.11	1.'247
D57	54	09	4434	0923	1155	34 39	15/15	00.09	01 01	207850	1.45	1.54	0.36	1.45	2.05	0.60	0.08	1,1256
D94	oi	0.0	1141	2001	1209	$44 \ 05$	14.56	00.07	NA	205335	0.72	1.72	1.00	0.64	1.92	1.28	0.11	NA
D94	0.5	00	1111	2001	1209	44 05	14 57	00.07	NA .	205325	0.75	1.64	0.86	0.78	1.76	0.95	0.10	1, 193
D94	16	(15	1111	2001	1212	46 03	$15 \ 05$	-00 02	NA	206000	0.80	1.70	0.90	0.70	1.50	0.50	0.10	1 249
D94	35	05	1111	2003	1215	49 11	15 11	-00-02	NA	206000	0.50		0.54	0.40	1.80	1.40	0.10	1, 254
D101	10	05	1111	0632	1124	26 05	15/26	-00.02	NA	212250	0.95	1.50	°0.55	0.95	1.70	0.55	0.07	1, 247
D101	4.2	10	1112	0633	1137	30 32	15 17	00.20	NA	209336	1.09	1:59	0.50	1.09	1.52	0.73	0.07	1,1254
D102	92	09	1121	0504	1159	31 36	15 - 27	00 06	NA	208685	0.87	1.49	0.62	0.56	1.77	1.21	0.09	1,7259
D103	. 11	11	5334	.0932	1059 -	19.29	15 18	-00 04	NA	215000	0.44	1.75	1.31	0.37	1.95	1.55	0.09	1, 249
D103	35	11	3111	0933	1115	23 44	15 32	00.05	NA	214500	0.53	1.85	1.32	0.51	2.03	1.52	0.09	1 1255
D103	57	11	1111	0935	1137	$31 \ 02$	15 18	00.23	" NA	209180	1.03	1.68	0.65	0.51	1.80	0.99	0.07	1 '260
D103	137	05	2111	0942	1227	60.49	14 19	-00 04	NA	214500	0.81	1,33	0.52	0.34	1.52	1,45	0.07	1.7235
D100	150	10	1111	0943	1228	61 34	14 26	-00 06	"NA	216000	0.50	1.51	0.71	0.35		.1.59	0.07	1 245
D103	169	10	1111	0944	1232	63 45	14 36	00 07	NA	223000	0.47	1.44	0.97	0.20	1.65	1.65	0.07	1. 246
D111	15	11	3111	2135	0940	07 11	14 53	-00 17	NA .	230500	0.55	0.95	0.10		1.44		0.19	1, 236

*All yaw values are determined from stellar readings.

Note NR denotes no reading made ~ NA denotes not available

D Max Rangé	0.44 - 2.13
D Min Range	0.27-1.49
Average D Max	1.66
Average D Min	0.83

Limiting

D Max Range	1.30-2.30
D Min Range	0.20-1.45
Average D Max	1,90
Average D Min	0.67

Gross Fog Range Average Gross Fog

					-							Terrair	٠ ،		L	imitin	g	
Pass	Frame	over- lap	Cloud	Univ. Time	Sun Time	Solar Elev.	Pitch (All Minus)	Roll	Yaw (All Minus)*	Alt. (yds)	D Min	D Max	7	D Min	D Max	Δ	Fog	Exp
D49	. 02	NR.	3311	2359	1307	NA	13555	-00°10°	NA	NA	0.67	2.24	1.57	0.30	2.35	2.05	0.11	1.124
D49	0.6	NR	3311	2359	1307	51'43'	14 05	-00 07	NA	206360	NR	NR	NR	0.21		2.04		1 '24'
D50	10 ·	05	4114	0116	1029	05 21	15 00	00 12	01:05	244719	0.64	1.23	0.59	0.64	2.06	1.42		1 (21-
D50	49	07	1114	0115	1116	14 36	$14 \ 52$	00.12	01 04	233726	0.75	1.61	0.56	0.55		1.21	0.11	1,1221
D52	.63	06	1111	0424	1220	31 51	14 44	00.25	01.42	211762	1.11	1.74				1.22		
D52	90	0.4	1111	0425	1229	35 39	15.06.	00.35	01 25	205772	1.41	2.21	0.80				0.21	
D53	12	04	1111	0552	1147	21 25	14 05	00 16	01 00	223759	0.79	1.92	1.13	0.67	2.04	1.37		1.1239
D53	62	04	1111	.0556	1232	36 45	14 50	00.26	NA	207145	1.23	1.97	0.74				0.21	
D54	0.9	00	2244	0719	1027	05.36	15 07	00.23	01.07	247955	0.49	0.75	0.26	0.35		0.45	0.10	
D54	50	06	1111	0723	1147	21250	14 26	00.53	01.53	222733		1.67				0.69		1 1239
D54	91	06	1111	0724	1155	20/44	14.25	00.51	01.39	219022		1.52				0.77		1 245
D54	107	06	1111	0725	1204	$25 \ 49$	14 39	00 45	NA	217022	0.60	1.60				1.34	0.05	

TOP SECRET RUFF

NO FOREIGN DISSEM

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					1			-		_		Terrai	n		I.	imitir	ng		
		77	.[1			Pitch		Yaw					İ		T			
Pas	Frame	Over-	Cloud	Univ.		Solar	(All	Roll	(All a		D	D	3	- D	- D	1.5	Fog	Exp	
		lap		Time	Time	Elev.	Minus)		Minus)*	(yds)	Min	(⊉lax	1 -	Min	Max	1			
D55	00	NR	5555	0549	1000	05°35"	15 02	-00 17	00-15	253602	NR	NR	NR	0.33	1.34	1 01	0.19	1.1206	
D55	10	0.5	3445	0550	1005	06 02	14 56	-00 19,	. 00 15	246516	NR	NR	NR	0.29	1.84	1.55	0.19	1, 206	
D55	90	NR	5555	05534		15 237	15/26	00.10	$01 \ 02$	227902	NR	NR	NR	0.86	1.35	0.52		1, 236	
D55	125	04	1111	0555	1159	24 27	14 42	00-10	01 - 14	219146	1.40	1.98	0.55	1.04	2.06	1.02		1,1234	
D55	164	0.5	1111	0556	1215	30 01	14 00	00.15	01 09	214201	1.20	1.79	0.59	0.73	1.95	1.22	0.05_	1, 249	٠
D55 D56	260 03	07 02	1211 1111	0900 1025	1244	42 35	15 20 .	00 06	00.57	205000	0.55	1.90	1.35	0.32		1.74		1, 255	
D56	61	06	2111	1025	$\frac{1149}{1214}$	29 52 29 52	15 04 14 46	-00 06 00 07	00 42	221745	0.27	1.43	1.16	0.27		1.25		1. 240	
- D61		·NR	4455	1504	1310	NA	14 24	-00 17	01 11 00 53	213492 205581	1.09 NR	1.57 NR	0,45 NR	0.99	1.67	0.55		1, 251	
D62	06	03	1111	1936	1314	42.54	14 29	00 05	NA	205000	0.70	1.31	0.61	$0.62 \\ 0.70$		1.20	0.09	1.256	
D62	07	0.3	1111	1936	1315	43 06	14 29	00.08	NA	205000	0.71	1.24	0.53	0.51		1.20		1.250	
D62	0.5	04	1111	1936	1317	43 19	14 30	00.07	NA 1	204650	0.56	1.24	0.68	0.56		1.25		1.251	
D62	09	04			-1315	43 32	14 30	00 07 -	NA	204500	0.52		0.90	0.30		1.57		1, 254	
D62	* 11	03	1111		1319	43 40	14 31	00 05	NA	204500	0.72		0.73	0.44	1.52	1.35		1, 255	
D62	22 23	02	1111	1937	1321.	45 05	14 23 >	00 02	00.46	204550	0.55		0.83	0.70				1,256	
D62	23 37	03 05	1111 1111	1937 1937	1321 1325	45 05		€ 00 03	00 46				0.54	0.40				1. 256	
D64	- 41	07	1111	2225	1125	,46 45 10 05	14 16 15 20	-00 06 -00 07	NA 01-25	204600	1.12		0.66	1.12		0.88		1.1256	
D64	65	05	2222	2252	1450	60.25	15 14	00.20	00 36	239425 275757			1.25	0.50		1.25		1. 224	
D65	24	06	1111	2359	1029	11 32	14 25	00 03	NA	239035			1.55	0.30		1.54 1.51	0.06	1.1157	
D65	54	05	1111	0001	1121	16 47	14 31	00 05	NA .	227365	1.49		0.57	0.59		1.27		1 236	
D66	69	04	4313	0134	1145	24 11	14 32	00.04	00 31	216000	1.41	1.94	0.53	0.25		1.66		1, 245	
D66	79	05	4313	0134	1151	25 21-	14 31	00-19-	NA T	217000			0.77	1.23		0.89		1.246	
D67 D67	26 50	06 09	1111	0259	1203	04 47	14 47	00 25	01 16	245400			0.66				0.17		
D61	54	05	1121	0435	1144	26 01 24 36	14 41 15 11	00 42 -00 02	00_45 NA								0.07		
D65	69	00 -	1111	0406	1152	26 56	15 13	-00 04	00-22	215378 215339			1.12 1.04					1, 243	
D05 .		0.5	1112	0439	1217	36 39	14 55	00 14	01 19	207000			1.45	0.68				1 247 1 255	
D68	167	07	2213	0440	1226	40 45	15 01	00 12	01 03	205550				0.37		1.71.		1, 257	
D69	12	06	1111	0604	1120	15 11	14 03	00.45	NA	227049				0.40				1, 251	
D69 -	46	0.9	1111		1122 *	23 29	14 05	00.06	NA	217449	0.50	1.71						1 254	
D70	14	10	1111		1126	19.59	15 01	00.31	01 23	222921 -		1.94.			2.04	1.49	0.21	1.239	
D70 D71	101 14	07.	1211		1215	35 54	15 23	00.24	01 02									1. 255	_
D72	25	11	1111 3121		1121	15 55 24 21	14 58 14 33	00 01 -00 10	NA 00/32									1 237	
D72	51	10	1111		1155			-00 03	NA								0.11		
D72	79	10	1112		1235		13:50	00 11	NA.									1.1256 1.1256	
D72	~9	10	1111	1046	1241		13 591	00 25	01.05									1, 256	
D75	. 00	06	1111 /	1947	1210	37 05	14 46	00 01	00 43						2.17			1, 251	
D75	30	05			1217			-00 05		1205500					2.23			1, 255	
D53	15	09			1133		14 45	00 05	00 31				1.70		2.07		0.15	1 246	
D53.	45 50	10 09			1151		15 05	00 21	ŊA									1. 251	
D55	16	07			1257 1120		15 03 14 12	00-21 -00-03	00 45				1.40 ~					1.'254	
D55	56 1	09			1141		14 34	00-24	NA NA									1,1241	
D55	55	11 -			1206			00 01	NA .								0.11_		
D56	33	05			1121			00 23	01 02							1.17		1,′254 1,′244	
D56	50	07			1153		14 49		NA .									1, 254	•
D56	95	05			1200		14 35,-	00-25	00 38 -		1.02	1.61 (0.59					1:1254	
D57	50	09			1128		14 52	00.00	NA			1.85 - 3	1.10	0.75	1.94 1	L.19	0.11	1, 245	
D57 D94		05			1155			00 05	01 01									1,1254	
D94 D94	07 22	06 07			$\frac{1209}{1212}$			00 07										L/248	
D94		07			1215			00 01 00 01	NA NA									L.1253	
D101		05						00 04	NA NA								0.11 : 0.07 :	L.1253 L.1246	
D101	47	07						00 27										t, 251 t. 251	
D102		NR				31 36	14 25	00-04										1.1255	
D103		10						00 03		218000 0								1/247	
D103		10						00.07				1.57 1	.29 (0.22	1.95 1	.76		.[258	
D103	91	10	1111	1935	1137	31 02	14 39	00/24	NA	209150 (0.75~ 1	1.55 (0.83 (0.75	1.80 1	.05	0.07 1	. '258	

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												Terrair	1	1	L	imitin	g	
Pass	Frame		Cloud	Univ. Time	Sum Time	Solar Elev.	Pitch (All Minus)	Roll	Yaw (All Minus)*	Alt. (yds)	D Min	D Max	Δ	D Min	D Max		Fog	Exp
D103 D103	141 154	05 10	$\frac{2111}{1111}$	0942 0943		60 49 - 61 34	15 35 15 26	-00 06 -00 04		214500 216000								
D103 D111	173 23	09 10	$\frac{1111}{3111}$		$1232 \\ 0940$		$\frac{15}{15} \frac{15}{94}$	00 11 -00 02		223000	1.05	1.95	0.87	0.62	2.10	1.45	0.17	

Note NR denotes no reading made NA denotes not available

Terrain

D Max Range 0.75-2.24 D Min Range 0.27-1.71 Average D Max 1.71 Average D Min 0.81

Limiting

D Max Range D Min Range Average D Max Average D Min 0.83-2.35 0.21-1.27 1.88 0.63

Gross Fog Range 0.06-0.21 Average Gross Fog 0.12

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NO FOREIGN DISSEM

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APPENDIX C. DENSITY READINGS

1. Stellar Index Camera

Density readings were taken on each pass, using a Macbeth QuantaLog Densitometer, Model

EP 1000, with an ET attachment and a 0.5 mm aperture. The values are correlated below.

					~	100		. •		
	Pass	Frame	D Min	D Max	Gross Fog	Pass	Frame	D Min .	D Max	Gross Fog
-	D49	01	1.56	2.99	0.34	D65	212	1.04	3,37	0.27
	D49	0.2	0.91	2.55	0.34	D69	213	0.65	3.04	0.27
	'D49	03	0.93	3.12	0.34	D69	229	0.95	3,27	0.28
	D50	0.4	0.50	2.54	0.31	D70	239	0.75	3.29	0.22
	D50	17	0.92	2.87	0.39	D70	244	1.06	3.35	0.24
	D52	15	1.64	3.45	0.25	D71	245	0.53	3.23 -	0.23
	D52	:34	0.99	3.17	0.28	D71	. 263	1.05	3.34	0.25
	D53	35	- 0.66	2.57	0.25	D72	264	0.95	3.34	0.24
	D53	55	1.42	3,39	0.32	D72	277	0.95	3.20	0.25
	D54	56	0.46	2.90	0.25	A72E	275	NR	· NR	0.27
	D54 ·	75 -	0.59	3.29	0.25	D75	277	1.24	3.45	.0.29
	D55	76	0.37	2.33	. 0.28	D75	254	NR	NR	0.24
	D55	11:3	1.14	3.30	0.25	D53	285	1.13	3.40	0.26
	D56	114	0.90	3.15	0.24	D53	296	1.51	3.61	0.24
	D56	123	1.07	3.27	0.25	D55	297	NR	NR	0.24
	A56E	124	$NR \rightarrow$	NR	0.25	D\$5	312	NR	NR	0.25
	A57	125	NR	NR	0.31	D56	313	1.04	2.56	0.25
	D61	126	1.24	3.29	0.27	D56	329	1.55	3.46	0.25
	D61	131	1.29 .	3.30.	0.24	D57	330	1.12	3.25	0.26
	D62	132	1.02	3.21	0.26	D87	345	1.17	3.43	0.35
	D62	137	0.69	3.10	. 0.26	D94	349	NR	NR	0.25
	D64	138	0.39	2.95	0.27	D94	355	NR	NR	0.25
	D64	145	0.56	≠ 2.97	0.30	D101	356	NR	NR .	0.25
	D65	149	0.56	3.21	0.27	D101	363	NR	NR	0.25
	D66	158	0.53	3,23	0.25	D102	364	NR	NR	0.25
	D66	159	0,28	1.44	0.27	D102	350	NR	NR	0.25
	D66	1.7.1	1,00	3,29	0.28	A103E	351	NR	NR	0.25
	D67	172	0.32	2,50	0.27	D103	352	NR	NR	0.25
	D67	186	10,95	3,10	0.25	D103	409	NR	NR	0.27
	Des	187	0.20	0.91	0.24	1				

Note NR denotes no reading made

D Max Range D Min Range $\substack{1.44 - 3.61 \\ 0.28 - 1.81}$

4.

Average D Max

Average D Min

3.11 0.91

Gross Fog Range Average Gross Fog $\substack{0.22 \text{-} 0.39 \\ 0.27}$

2. Terrain Index Camera

Density readings were taken on each pass, using a Macbeth QuantaLog Densitometer, Model

EP 1000, with an ET attachment and a 0.5 mm aperture. The values are correlated below.

Pass D49	Frame	D Min	D Max	D.14	T	
D10			1 2 3144	D Min	D Max	Gross Fog
	01	NR	NR	- 0.34	1.73	0.05
D49	02	NR	NR	0.20-	1.77	0.10
D49	03	· NR	NR	0.13	1.74	0.11
D 50	04	0.16	0.67	0.16	0.91	0.10
D50	17	0.15	1.12	0.15	1.12	0.07
D52	18	0.30	1.01	0.30	1.01	, 0.10
D52	34	0.40	1.47	0.16	1.47	0.07
D58	35	0.17	1.08	0.17	1.05	0.09

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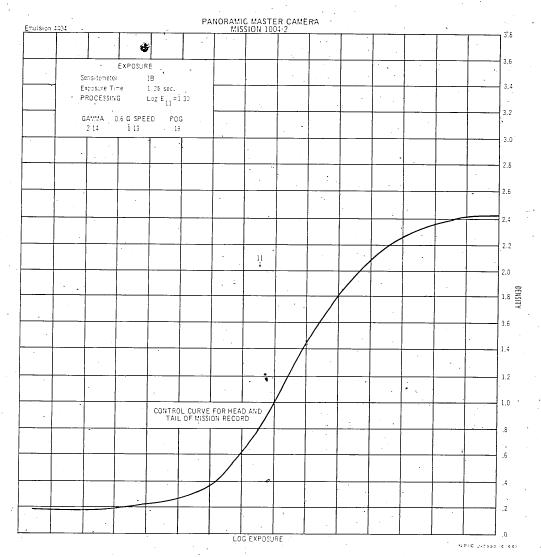
		Terrain			Limiting	
Pass	Frame	D Min	D Max	D Min	- D Max	Gross Fog.
D53	55	·NR	NR	NR	1.58	0.07
D54	64	0.31	0.55	0.31	0.88	0.07
D54	- 75	0.47	1.35	0.47	1.35	0.07
D55	82	0.25	0.74	0.25	0.57	0.07
D55	113	0.31	0.295	0.31	1.58	
D56	114	0.25	1.10	0.25	1.13	0.07
D56	123	0.26	1.00	0.26		0.07
A56E ~	124				1.10	0.07
A56	125	NR	NR	NR	NR	0.07
		NR	NR -	NR	' NR	0.07
D61	126	NR	NR	. 0.66	1.29	0.08
D61	131	-NR	NR	0.43	1.54	0.08
D62	132	0.25	×0.95	0.25	0.98	0.10
D62	137	0.14	0.91	0.14	0.91	0.10
D64	142	0.18	0.70	(LA 6	0.85	0.12
D64	148	NR	NR	0.15	1.47	0.11
D65	149	0.34	0.67	0.20	0.70	0.11
D65	156	0.53	1.05	NR	NR	0.11
D66	163	0.33	1.15	0.22	1.15	0.07
D66	169	0.40	1.35	. 0.15	1.36	0.07
D67	177	0.23	1.21	0.23	1.21	0.07
D67	155	0.23				
D68	193		1.09	0.17	1.18	0.08
		0.25	1,29	0.25	1.29	0.07
D65	212	0.60	1.22	0.52	1.24	0.07
D69	213	0.20	1.02	0.20	1.06	0.07
D69	229	0.29	1.25	. 0.29	1.45	0,07
D70	230	0.15.	1.31	0.15	1.31	0.07
D70	244	0.30	1.50	0.30	1.50	0.07
D71	245	0.33	0.87	0.33	1.14	- 0.07
D71	263	0.34	1.09	0.13	1.46	0.07
D72 .	264	0.23	1.12	0.14	1.12	0.07
D72	277	0.31	1.06	0.31	1.06	0.07
A72E	275	NR	NR	NR	NR	0.07
D75	279	0.44	1.49			
D75	254	NR		0.44	1.49	0.07
			NR	NR'	NR	0.07
D53	255	0.17	1.17	0.17	1.17	0.07
D53	296	0.27	1.10	0.15	1.37	0.07
D55	297	0.22	1.17	0.22	1.17	0.07
D55	312	.0.39	1.31	0.26	1.31	76.0
D56	319	0.27	1.17	0.27	1.17	0.07
D56	326	0.49	1.24	0.49	1.24	0.07
DS7	330	0.24	0.90	0.24	0.90	0.07
D57	345	0.27	1.55	0.27	1.58	0.07
D94	349	₹0.17 ·	1.05	0.17	1.05	0.07
D94	355	0.27	1.05	0.17	1.05	0.07
· D101	356	0.25	1.22	0.25	1.22	0.07
D101.	363	0.55	1.30	0.55	1.30	0.07
D102 -	372	0.33	0.65			
D102	250	0.23		0.31-	1.07	0.07
			1.64	0,23	1.64	0.07
A103E	851	NR	NR	NR	NR	0.07
D103	409	0.55	1.17	0.22	1.17	0.07
A104E	410	NR	NR	NR	NR	0.07
D111 .	411	NR	NR	0.07	0.30	0.07
D111	4.25	0.39	0.89 *	0.39 :	0.89	0.07

Gross Fog Range Average Gross Fog 0.05-0.11 .- 18 -

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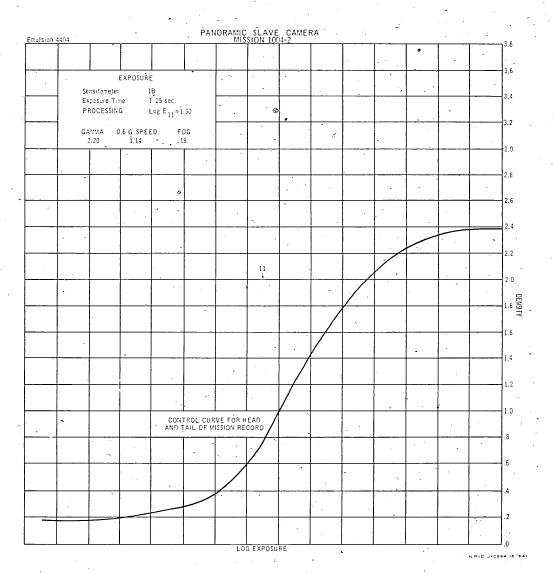


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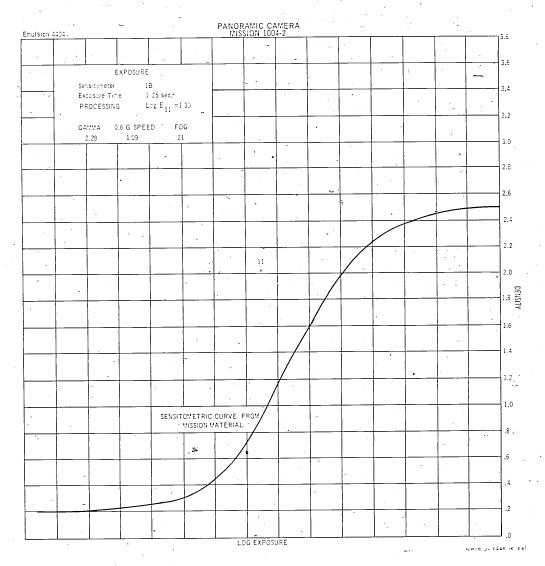


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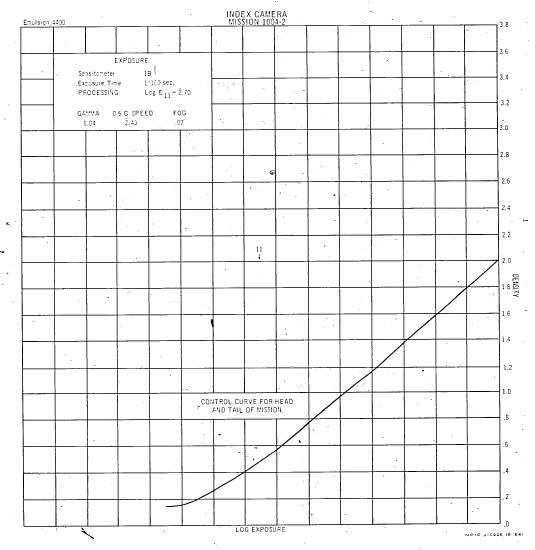
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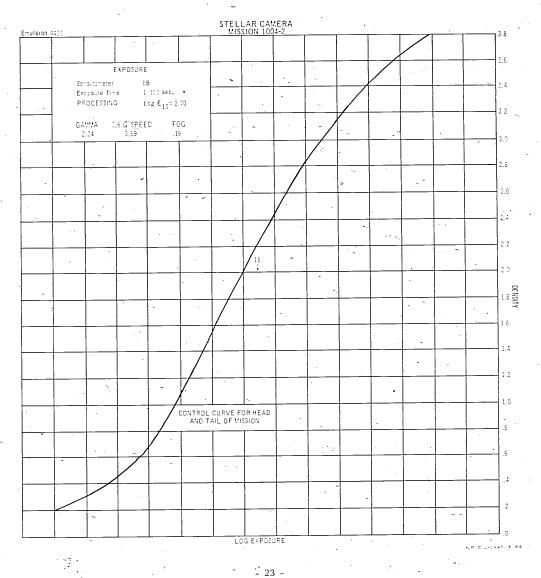
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APPENDIX D. EDGE SPREAD FUNCTION

In an attempt to establish an objective measurement of image quality in photography, the technique of obtaining the spread function from microdensitometric edge traces is being investigated. The spread function curve represents the whole photographic system, and is a summation of the separate elements: lens, film, and uncompensated image motion due to vibration, velocity, roll, pitch, yaw, and aerial turbulence.

To assign a single number to the spread function, the width is measured at 50 percent amplitude. This number, usually expressed in microns, may be converted by use of the scale factors to ground distance in feet.

Edges meeting the criteria described below have been found in domestic passes of missions in the same frame as resolution targets and have been scanned. The ground distance in feet, thus determined, has been close to that determined from the resolution target. Although the techniques used are not refined and are considered to be still in the development stage, the potential of this type of objective analysis should be realized. The two examples of edge scans and their respective spread functions are included as a preview of this type quality analysis.

Any optical image can be thought of as being composed of an infinite number of image points (or lines) of light, each being conjugate with points (or lines) in the object. While the object points can be infinitesimal light sources, the image points are always mounds or distributions of light having finite size. This blurring of light points in a photographic system comes from diffraction and aberration in the lens, light spreading and diffusion in the emulsion, and image motion caused by camera movement and atmospheric shimmering. The fundamental building block of the image then is the distribution of light in any of the image points. This

distribution is called the spread function of the photographic system.

Lamberts and others have explained the mathematical and experimental correspondence of a sharp edge and its spread function. An analogy exists in the techniques of studying electrical system response. The analysis requires that the source or object fulfill the conditions of a unit step function, i.e. exist for an appreciable time or distance at a fixed signal level and instantaneously or abruptly change to a new level which is maintained for an appreciable time or distance. The spread function is obtained by differentiating the signal output curve point by point (i.e. measuring the rate of change or signal with time or distance, and plotting signal amplitude versus time or distance).

As a starting point the mission is examined to locate examples of best photography with edges long enough and straight enough for use in the microdensitometer, and having uniform density on each side of the edge to fulfill the conditions of a unit step function. This requirement is usually achieved by rooftops of buildings in large-scale photography, and aircraft runways in small-scale photographs.

The microdensitometer used is a Joyce-Lobel Double Beam Model III C. It is used with an effective slit of one micron by 125 microns. The recording table and sample table are directly linked with a ratio arm of 1000:1. The speed of the scan is variable and is determined by the amount of pen deflection (as the pen is deflected the speed decreases giving the pentime to reach its maximum response). The chart thus produced represents a plot of chart displacement versus distance. This plot is manually smoothed by the analyst and is a judgment of what the edge would be if grain and other anomalies were absent.

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The data reduction is done manually at present, but the feasibility of using the UNIVAC 490 computer is being investigated. The microdensitometer calibration curve (chart displacement to density) is used to determine the densities at equal distance increments along the trace. The D Log E curve for the material (density to log exposure) is used to determine the Log E and therefore the exposure required to produce the determined densities. The values

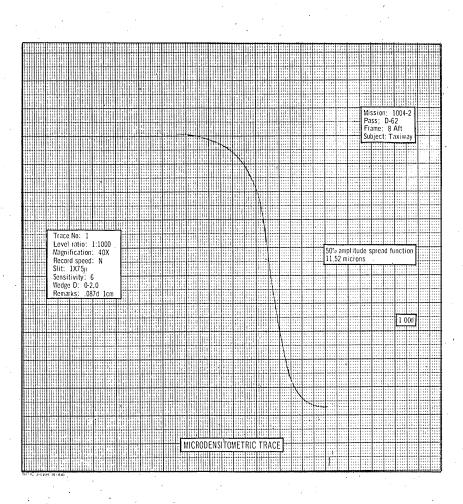
of E are plotted against the distance across the edge to produce the original scene reflectance distribution as recorded in the negative. The final step is a determination and plotting of the slope of this curve (dE/dX) versus distance, point by point. This last plot is the spread function for the whole photographic system.

The width of the spread function curve is measured at 50 percent of maximum amplitude and is indicated on the enclosed traces.

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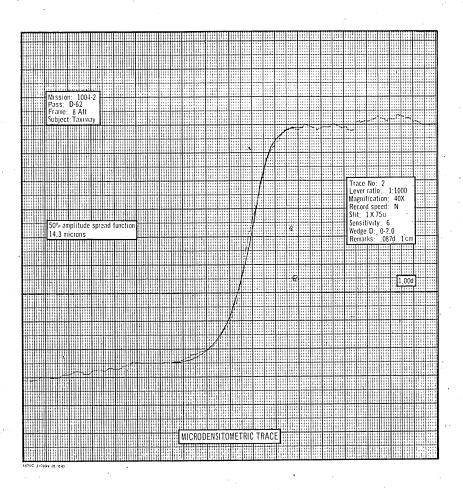
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APPENDIX E. MISSION COVERAGE STATISTICS

1. <u>Plottable Coverage</u>: The following is a summary of plottable coverage for this mission given in linear nautical miles (ln/nm) and in square nautical miles (sq/nm). The figures are the sum of both master and slave photography, and exclude coverage which is entirely over water or completely cloud covered.

In Table 1, a mean cloud percentage value has been calculated for each category for use in determining a combined cloud-cover percentage for all operational passes of the mission.

The occurrences of each cloud category within an operational pass is expressed as a percentage and appears in Table 2. Each percentage is a ratio of the number of occurrences of a given cloud-cover category to the total number of cloud observations in a photographic pass. For example: if the number of category 1 occurrences in a given pass is 200 out of a total of 1000 (250 frames x 4 quarters), all categories combined, then 20 percent of the pass would be as in category 1.

A cloud-cover percentage per pass is included in the last column of Table 2 under "cloud-cover percentage per pass." This value is determined by the summation of the products category percentage in each pass and the mean cloud percentage for that category as established in Table 1. For example: it is determined that the following percentages exist in a given pass:

 20 percent
 Category 1

 15 percent
 Category 2

 30 percent
 Category 3

 25-percent
 Category 4

 10 percent
 Category 5

Then, by using the mean cloud percentage established in Table 1, the following computations are made:

0.20 x 5.0 = 1.00 percent 0.15 x 17.5 = 2.63 percent 0.30 x 38.0 = 11.40 percent 0.25 x 75.0 = 18.75 percent 0.10 x 100.0 = 10.00 percent TOTAL 43.78 percent

Hence, 43.8 percent of this pass is cloud covered.

2. <u>Cloud Cover</u>: This statistical analysis of cloud cover on Mission 1004-2 is based on cloud cover per quarter segment of each frame of photography. The data are obtained by analysts trained in estimating cloud cover by designated categories.

Five cloud categories have been formulated for use on this photography. These categories allow for the wide latitude of cloud-cover conditions commonly found on a frame of this photography.

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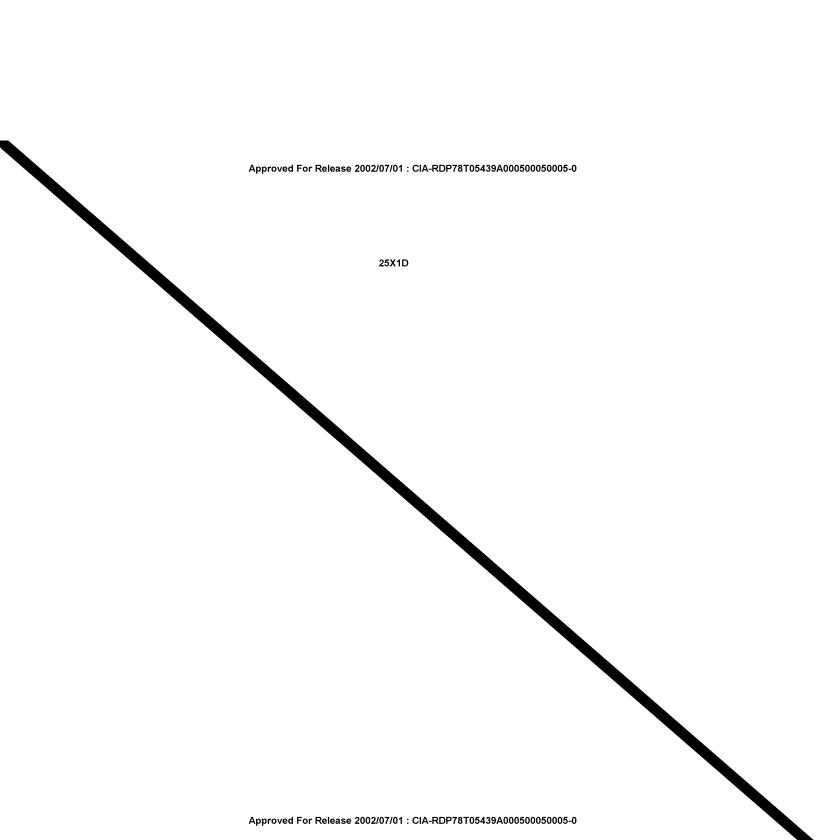
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Category Number	Percent of Cloud Cover	Description	Mean Cloud Percentage
1	Less than 10	Clear	5
2	10 - 25	Small Scattered Clouds	17.5
3 '	26 - 50	Large Scattered Clouds	35
4	51 - 99	Broken or Con- nected Clouds	.75
5	100	Complete Over-	100

Percentage of Cloud Cover Categories by Passes

Pass Number	1	2	3	4	5	Cloud-Cover Percentage Per Pass
50 D	60.6	18.5	12.5	8.1	0.0	17.2
52D	85.9	8.8	3.9 .	1.4	0.0	8.4
53D	31.3	5.7	5.4	7.5	50.1	60.4
54D	62.2	7.3	9.1	11.8	9.6	26.3
·55D	25.5°	20.5	14.9	24.6	10.9	40.1
56 D	40.1	10.9	13.7	21.6	13.7	39.0
64D	21.7	35.6	22.8	13.9	3.0	29.9
65 D	60.3	3.0	4.7	23.3	8.7	31.5
66 D	44.9	13.7'	20.5	20.9	0.0	28.1
67D	69.5	4.6	5.7	19.9	0.0	21.3
65D	55.3	18.9	9.0	10.9	2.9	20.7
69 D	72.3	19.7	5.9	2.1	0.0	10.9
70D	62.7	10.4	4.0	20.4	2.5	24.3
71D	10.7	7.5	11.4	22.2	48.2	71.0
,72D	56.3	20.3	15.6	6.7	1.1	18.4
83D	79.0	10.2	6.2	4.6	0.0.	11.5
85 D	65.3	17.3	9.1	8.1	0.2	16.0
86D	47.2	6.4	3.4	17.6	25.4	43.4
57D	30.4	9.9	11.4	21.8	26.5	50.5
101D	47.9	40.6	4.5	6.6	0.4	16.5
102D	40.5	9.6	6.2	24.2	19.0	43.3
103D	39.5	14.3	10.9	16.5	18.8	39.5
111D	35.6	37.1	9.3	5.0	0.0	16.2
112D	12.0	8.8	5.6	71.3	2.3	60.0
	48.2*	14.3*	9.6*	15.6*	12.3*	*32.5**

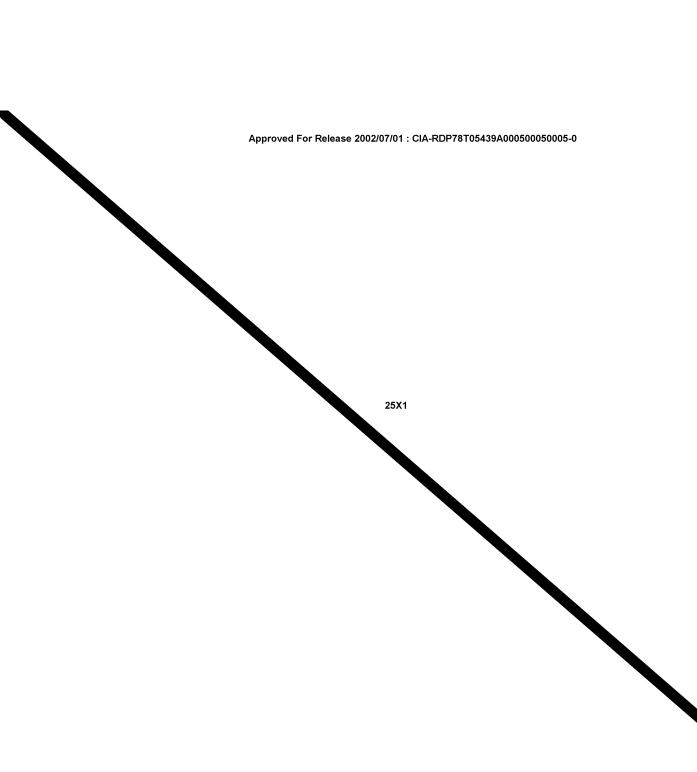
^{*}Average Percentage by Category for Mission.
**Overall Mission Cloud Cover Percentage.



TOP SECRET

TOP SECRET

Approved For Kelease Zuoziorius z SiAskus ro rusasannius initiativa saara



1	PASS	DA							SDI			SECRET LING REG		-D			. 1			
,	32A	2.0) 97	<u> 7 62</u>					, 511			·	- 1					· · · · · · · · · · · · · · · · · · ·		
w .	FRAME	1		TIME	TIME Diff	ļ	CAMER/ Latitude	NADIR	ongitudo		FURMA I itude	CENTER Longitue	de .	ALTITUDE (ft)	VELOCITY (ft per sec)	AZIMUTH deg min	SUN ANGLE	PITCH deg min.	ROLL deg min	
		hr	min	50C	milsec	deg	min	deg	min	deg	min		min				<u> </u>	L		-
	3.			27,517	4.0****		51.540		-20 . 546		üöll.	976 2		1258424 1258466	293 31 233 37	623 51 624 65	14:47 14:57			
	2			23,086	5870		12,127		44.15E		26N 46N	-076 4 1676 5		1247646	23343	324 17	15 36			
	3 '			28,991	5595 6636		31.70R		57.09 E 11.16E:			777		1244959	235401	124 30	15 16			
	4			44,296	5315		90,28N 30,68N		24.51E		25K	3077 S	in the	1242295	23355	024 42	15 25		*	
	. 5	1	29	49,566	52.73 51.63		26.73N		137.62E		4211	077		1239673	23350	324 55	15 33			
	`6 7			54,746	5185 5155		44 n 67 H		51.27b		4311	677 5		1237061	23366	925 9 7	15 42	.*		
		5 / JL	27	59,0001 05,041	5140		92.53N		64.07E		16H	678 0		1236455	25371	025 26	15 51			
	9			13.136	5095		25.231		18.56E		35M	970 1		1201600	23377	-25 33	16 65	·.		
	10			15.201	15065		37.7411		32.36E		53%	678		1229295	29302	005 46	16 08			
	11			20.231	9930		55.148		46.28E		1111	878 4		1226737	23380	JE5 59	16 17		/	
	12			25,251	5023		12,478		09.37E		2011			1224102	23393	126 12	. 16 25			
	13			30,221	4970		29.59/1		14.53E		46H	079 1		1221651	23399	026 26	. 16 33			
	14			35,176	4955		46,6411		28.36E		фэN	679 3		1219125	25/904	626 39	16 42			
	1.5			40,096	4920		63.53N		43.301		2611	079 4		1216015	2341.9	026 53	16 50			
	16			44,996	4980		25-63211		57.09E		37ñ	079 5	7E	1214134	23415	-627 97	16 58			
	17			49.861	4865		36,978		12.60%		5411	080 1		1211620	23420	627 21	17 56			
	13			54,691	4630		53.46N		27.40E		1111	680 2	7E	1209155	23425	027 39	17 14			٠,
	19		30		4813		09.85%		42.41E		2.7ia	1000 4		12.6696	23431	027 49	17 22			
:	2.0	-:1		04.3:1	4800		26.178		57.59E		446	000 1	7E.	1244241	25436	120 u4	17 35	1		
	21			09.071	4776		42.36N		12.000	55	$\emptyset3\%$	- #81. I	26	1251 7 97	23441	520 L8	17 38			
	22			13.331	4753		58.47N		28.410	. b5	15B	931 8	lok	11.99557	23446	:C28 33	17 45			
	23			18.562	4730		14.4611		44,06E		328	661	31	1196235	25452	625, 48	17 50			
	24			23,276	4715		304358	031	59.59E	55	4511	601:	9h.	1114512	23457	529 63	18 51			
	25			27,966	4690		46.138		15.COE	56	Doit	902 1	DE.	1102104	23462	#29 19				
	26			32,642	4675		01.02N		32.070	56	2001	002 3	2E	1100705	23457	929.34				
	27			37,206	4645		17.37N	082	46.40E	56	$J \subseteq \mathbb{N}$	662 7	OL.	1167316	25472	H29 50				
	28			41.926	4640	57	32.86N	080	04656E	56	1.214	303 L		1104990	2.3477.	- 650 - 6 6				
	29	. 1	31	45,501	1 4655	57	40.20N		21.65E		07N.	303		1102201	23462	038 22			4.	
	3.1	01	31	51,131	4633	58	33.46N		33.56E	57	238	303 1		1130194		030 38				
	31			55.696	4565		18.618		55.656	57	JCN.	0000		11,77044	23493	636 55				
	32	01	. 32	256	4563	56	33.66N		12.94E		5514	034 3		1175495	25498	0.31 11			**	
	33			64,006	4550		40.6711		30.47E		SSN			1170151	20503	501 23			. '	
	- 34	01	32	09.341	4535		,13 . 53N		48 . 226	,	2411	$G_0 Z_r = C_0$		1173313	23558	1031 45 100 10				
	- 35	01	32	13.356	4515		18.370		06.176		3914	505 1		1160406	23513	. p32 93				
	36	0.3	32	18,366	4513		33.10N		24.38E		5411	# # # # # # # # # # # # # # # # # # #		1166168	123518	1032 20				
	-37			22.852	4405		47.711		42.70E		#UN	005 4		1163046	23525	032 36				
	38			27.326	4475		02.23N		01.42E		2011	656		1161537	23528	032 56				
	39 .			31.701	4455		16.65M		20.270		38N	086		. 1159237	23533	. #33 .15				
	4.			36.227	4445		30.98N		- 39.30E		5211	300		1156940	23538	033 53				
	41			40,646	4420		45.19N		. 58 . 68€.		'U711	19561		1154565	<u>つき</u> づちんよ	635152		44		
	42			45 . 62	4415		59.33N		10.26E		214	. 657 .		1152536	23547	034:11				
	43	01	02	49,466	4405	61	13.080	⊕87	38.12E	60	3511	- 037 :	ici.	-1150105	23552	£34 30	- 20 16			
									1.0							:			£Ŗ	

									TOD	CECDET						
	PASS	DAY MO		1				SPI	,	SECRET	PED .					
	331	20 04		TIME		CAMER	A NADIR			T CENTER	·	VEL OCITY	AZIMUTH	SUN ANGLE	PITCH	ROLL
	FRAME	. Z hr min	TIME	Diff		Latitude min	L	ongitude min	Latitude deg min	Longitude deg min	ALTITUDE (ft)	VELOCITY (ft per sec)	deg min	SUN ANGLE deg - min	deg min	deg min
	1		59,267	mirsec		50.99N	655	35.65E	52 377	095,090.	1225777	20396	025 56	16 88		
	2		05.057	5790		-10.99N	055	51.506	52 2714	355 51E	1222221	23096	ψ26 1 1	16 18		
	3		16,392	5335	50		ØĐĄ	SG .A9E	52 46N	9556, 06E	1220115	23452	-926-25	- 16 27		, .
	I_1		15.596	5235	53	47.281		21.95E	53-94N	356° 21E	1017432	23400	126 40	16 56		
	5	03 02	25.767	5179	54	35.03N		36.74E	- 93 H2N	p56 36E	1244625	23413	-026 54	16 44	4	
	6	.::3 02	25,086	5120	54			-52 . 62E	50 39N	g56 52E	11212212	20419	327 09	16 53	A	
	7	53 _, 02	30,001	5.75	54				93 571:	357 57E	128 9620.	25424	127 23	17 01		
	3		35.991	5008	54		057	22.69E	34 1411	057 22L	1227049	20430	- 02 7 -38 - 02 7-53	-17 10 -17 10		
			40,996	- 500E.		14.150	. 657		54 32N	- 00 7 30L,	1264469° 1264942	23435 23441	- D28 D8	17 26		
	110		45.971	4975.	. 55			54,54E 15,32L	154 498 155 06R	- 657-54E - 658-16E	1199465	23446	1.23 23	17 94		
	11		50,926 80,637	4955	- 55 - 53	47.878 04.49N		26.416	55 22R	950-260	1196886	13452	J28 39	17 42		
	12 13		55,636 -0,736	4910 4900		21,331		42.720	1 55 39N	050 426	1154076		1020 54	17 59	7.7.46	
			05.6.2	4865		37.42N	(15.8	39.17L	55 56N	858 59L	1191000	23462	329 10	17 58		
	14 15	4	1. 451	4850		53,7211	659	15,026	. 56 12N	059 115E	1160391		329 26	18 06		
	16		15,267	4015	57		059		56-25N	OSS JZE	1166916	23475	3029 42	18 14		4.
	17		27.166	4800		25.911		49.648	9514911	- 659 49t.	1104452	23476	029 59	18 22	1	
	16		24.826	4760		41.78N		(16.738	57 5174	-660 56E	1182005	234541	036 15	10,30		· v ·
	19		29,576	4750		57.581		24.15E	57 1.70	060-24L	1170562	23489	030 32	18/37		
	20		34.286	4710	50	13.210	969	91.65E.	57 33h	J60 416	14.77136	23494] DS9 [49]	18 45	•	
	21	93 93	986.86	4750	58	28.768	960	59.40E	57 46N	060 50E	1174720	20495 (31.6	18 52	•	
	22	33 331	43,666	4660	. 53	44.201		17.05C	58 GAR	Q61_17L	1172310	20504	031 23	19 00		
	, 23-	35 93	43.326	4666		59.52N	961	35.51L	58 ZEN	· 061 35E	F1109910	23510	931.41	19 37	· .	
	54	93,33	52 , 96 1 ,	4635.	. 59		661	,	58 3511	061 531.	1167522	29515	551 58	19 14		
	25		57,596	4535	59		0,62		53 50h	062 12E	1165100	23520	032 17	19 22		
	26		02.196	4623.		44,673	062		59 Jori	062 31E	1162762	20525	1032 35	19 29 -		1,
	. 27		36,796	46.00	-59		F62		59 316	- 062 50E	116 (390	2353 .	32 53			٠.,
	28		11.356.	4570		14.6111		09.73E	359 36h	300 1000 061 1000	- 1155553 - 1155631	23555 23540	- 533- 1 2 - 633-3 1	19 43 19 56	1.	
	29		15,926	, M560		-29.32N -43.89N		29.29E 49.04E	- 59 51R - 60 35R	- 06J 296 - 963 49E	1153045	25545	033 50	19 57	٠.	
	-30 °		20.456 24.977	4530 4520	- 60 - 603		064		60 20R	564 59E	1151.15	23550	-334 10	20-84		
	31 32	:13.94 - 35.94	29,471	- 4495.		12.71N		29.32E	1 58 Joh	364 29E	1140690	23955	034 30			
	33		33,961	4498		26.99h	064		(45 45)	964 49E	1146372	23560	034 50	20 18		
	34		38,426	4465		41.138		10.630	51 0444	035 10E	1144067	123565	235 10	20 25		
	. 35		42.886	4460			965		61 166	\$65 31E	1141764	23570	J35 30	20/31	1 1	
	36.		47.321	4435	62		065		61 3211	065 53E	1109474	;23575	4035 51	20 38		t
	37		51.761	4449	62	2,3 a 100	266		61 460	7005 14C	1137130	23560	336 12	20 45		
	. 38		56,176	4415	62	36.76H	066	36.64E	62 SWN	066 96E	- 1134989	23505	536 34	20 51	1	
:	39	103-95	J.581	4405	62	50 a 44 R	066	50.687E	52: 14H		1152025	23590,	936,56	20 58		
	40		64 . 966 -	4305		03.98N	667		62 28H	067 218		23595	237 18	21 04	1.	
	41		39.346	4388	THEORIE.	17.45R		44.2 E	62 42H	067 44E	1123395	73600	037,40			
	42		13.696.	4350	6.5		260		62 55M	268 17 7 0	1125851	23695	38 92			
	43		18,041	4345	63			30 " 60L	63 59N	068 30E	1123637	23610	658 25			
	44		22,366	4325		57.04N		54.37E	63 22N	1. 1. 1	1121574	23615	- 038-49 - 039-12			
	45		26:676	4310		10.01N		18.37E	- 63/35N -179 arm		1119140 1116931	23619 23624	039 36			
	46 7.7		971	4295		22.67N		42,68L	- 63 46N - 64 01N			23629	- 957 50 - 540 66			
	47	00 95	35,261	4290		35.64N		97.96E						₩ - 72		14.7
	Hans	lle Via				Approved	ror b			SECRET	T05439A000	າວບບບວປປເ	/3-U		. 1	

Handle Via TALENT-KEYHOLE

TOP SECRET

SPECIAL HANDLING REQUIRED

<u> </u>	PASS		O YR			ð	SPE		ECRET LING REQUIR	ED		·			
L F	33A RAME	z	TIME	TIME Diff	Latitude	ERA NADIR Longitu		FORMAT Latitude deg min	CENTER Longitude deg min	ALTITUDE (ft)	VELOCITY (ft par sec)	AZIMUTH deg min	SUN ANGLE deg min	PITCH dog min	ROLL deg min
F -	68 49 56 51: 52 53 54 55 57 58 59 61 62 63 64 65 66 67 68	min min	39.536 43.612 48.162 52.397 56.531 68.751 68.751 69.146 17.491 21.642 25.791 26.526 34.057 38.176 42.286 46.341 56.476 56.616 72.671	Diff milsec 4275 4275 4250 4265 4220 4230 4175 4175 4150 4150 4150 4055 4055 4055	deg min 64 46.35 65 35.86 65 13.31 65 25.64 65 49.34 66 13.77 66 25.67 66 37.11 66 40.38 67 40.38 67 44.22 67 54.97 68 45.66 68 46.7 69 46.67 60 36.66 65 46.7 65 46.7 66 46.7 67 36.66 66 46.7 68 46.7 68 46.7 69 46.7 60 36.66 66 46.7	deg deg	min	dej min 64 14R 64 14R 64 14R 64 12R 65 12R 65 12R 65 14R 66 14R 66 14R 66 14R 66 15R 66 15R 67 15R 67 15R 67 15R 67 15R 67 15R 68 14R 69 15R 67 15R 67 15R 67 15R 68 14R 69 15R 60 15R 60		1112569 111003 113011 1105520 1130740 1101564 105520 1957236 1055007 1007937 1007074 1070074 1075978 1075978 1077971 1077971 1077971 1077971 1077971 1077971 1077971 1077971 1077971 1077971 1077971 1077971 1077971 1077971	23634 23649 23649 23649 23649 23667 23667 23672 23684 23691 23686 23719 23724 23716 23714 23716 23714 23719 23714 23719 23714 23719 23727 23727	040, 25 041, 15 041, 15 041, 15 041, 15 042, 07 043, 09 043, 09 043, 09 044, 19 045, 19 046, 16 046, 47 047, 18 047, 18 049, 23 049, 23 049, 23 049, 25 049, 25 049	21 95 22 97 22 97 22 19 22 25 22 31 22 36 22 42 22 48 22 54 22 59 23 15 25 21 25 27 25 27 25 37 25 38 25 38 25 48 25 48 25 48 25 48 25 48 26 25 27 23 32 28 38 28 38 38 38 38 38 38 38 38 38 38 38 br>38 38		
	-70 -71 -72	- 33 F	761 761 761 761 761 761 761 761 761 761	4035 4035 4276	69 66.4	IN 281 57	61E	68 45N - 56 55N	901 925 902 295	1063500 1061312		051 36 .52 12		•	ž .

										T	OP S	SECRE	CRET								٠.		
	PASS 330	20 04 62			,			SPE	ECIAL HANDLING REQUIRED				3			1					_		
	FRAME			TIME Diff mil sec	CAMERA Latitude deg min		NADIR Longitude deg min		FORMAT Latitude deg min		CENTER Longitude deg min		ALTITUDE (ft)	VELOCITY (fi per sec)	AZIMU1 deg m	in	SUN Al	min	PITCH deg min		ROLL deg min	_	
	1			00,621	4395		27.98H		12.86E.	65 68	52N 39N	169		639 7 25 80 793 8	24243 - 24247	$\frac{138}{138}$	12 39	- 35 - 35.					
	3	3 .3	15	13.47 16.881	3865	65	33.33N	173	04.40E	65	28H	170	946	836 37 2 8548 77	24251 24254	139 139		.00 39					•
	4	.03 -03		24.236	3 7 65 3650		52.16N 41.16N		127.19E 49.25E		16N 96N	176 176	496.	803469	24257	139	4.5	30	13				
	. 6	63	15	27.836 31.421	3669 3585		19.14N 19.16N		13.71£ 31.73L		55H 44H	171 171	ICE ME	031966 838535	24261 24264	140 149		30 30	14				
		. 63	15	34,0977	3555	64	00.22M	171	52,37U	64	Self Ban	171 172	52E	529125 82 7715	29267 24270		48 38	739 39					
	9. 181			30.521 42.046	3545 3525	6.3	5 7. 25N 46.35N	172	12.67E 32.56E	64	1.144	172	320	1 026323.			27	اززد . 9د	16				
	11 12	93		45.562 49.862	35 1 5 35 0 3		35,32N 24,35N		52.14E 11.67E		95W 49M		11t.	523567	24280	142	05	30	16				
	13	03	15	52,551	3498 34 7 0		.13.36N 02.36N		30.30C 40.07E	. 63 63	3611 2711		50 t. 40 t.	322204 323853	24263 24286	142 142		30 30	17 17		٠	.,	
	14 15	2	15	56.021 59.491	3470	62	51m36N	1.74	97.2JE	63	178	174	070 25E	319568 315176	24259 - 55292	143 143		38 30	17 17		•		
	16 17			02,941 06,381	9459° 9446°		40,35N 29,34N	174	25.2KE 42.01E	7.2	Mon: Nec	3.74	406	816852	24295	143	34	30	17	i e			
	18	53	1.6	09.801 13.216	3429 3415		18.35N -07.33N		90.30E 17.44E		44N 33N		03E 17E	815541 814257	24298 24301	143 144	38	30	17 13	,	-		
	2.5	193	16	16.616	3400	61	56.32N 45.20N	175	-34.29E -30.91E		22N 11N		34E 59E	512944 31165 7	24304 24307-	-144 -144			18 18				٠.
	21 22			23,396	3395 3385	6Î	34,26N	1.76	07.286	52	ach.	175	71	aljoss 859111	24316 24313	144 145			18. 17				
	23 24			26.771 30.136	3375 3365		23.22N 13.17H	176	. 23 . 39€ . 39 . 27E	51	49N ,30N	176	23E 35E	. 607651	24316	145	28	50	17 17				
٠.	25	63	-16	,23.501	3365	61	31.09N	176	54 . 956	61	278	176	54E	83659 <u>6</u>	243 1 9 :	143	40	الوف	3.1				